

# Modelling of Dislocation Bias in FCC Materials

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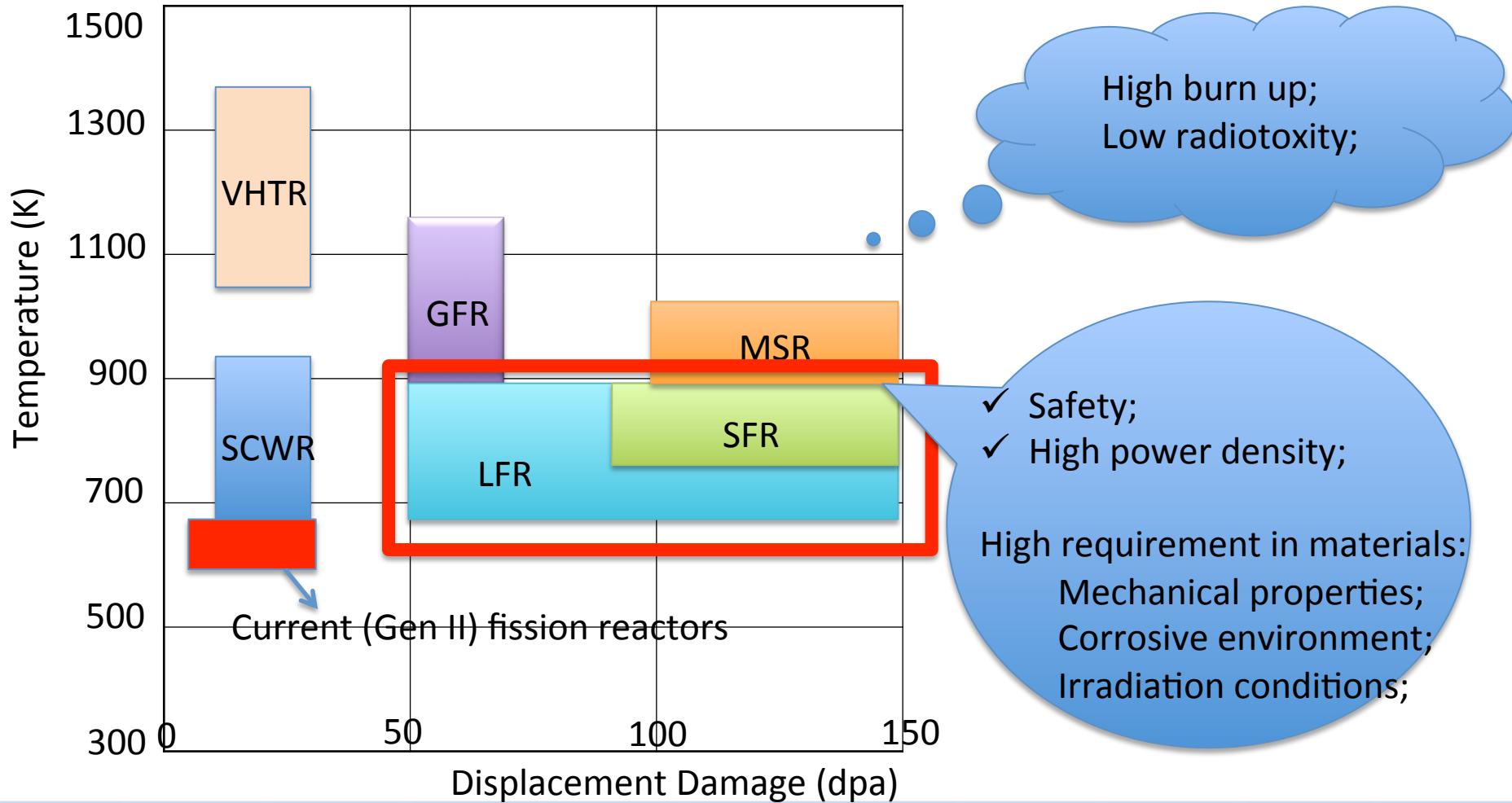
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  - Gen IV and Austenitic steel
  - Swelling
  - Bias
- Methods
  - Standard rate theory
  - Theoretical approaches
  - Analytical interactions
- Results
  - Interaction energy
  - Bias factor
- Conclusion

Why?

How?

What?

# Why? – Gen IV



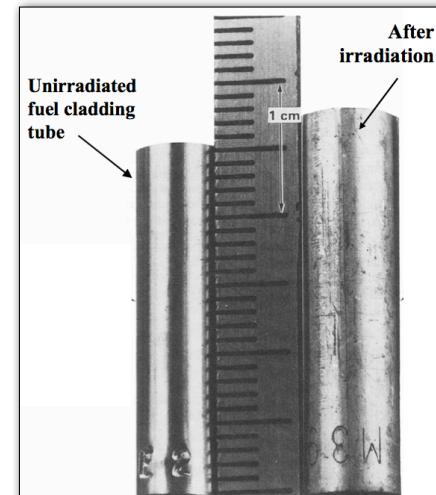
# Why? – Austenitic steel

## ➤ Austenitic steel

- ✧ Fe-Cr(15-20%)-Ni(8-15%)  
FCC
- ✧ Good strength and ductility,  
fatigue resistance, little or no  
precipitation, stable parent  
austenite phase
- ✧ Swelling
  - ✧ 260% swelling in 316 during  
proton irradiation

Properties of 316L Stainless steel

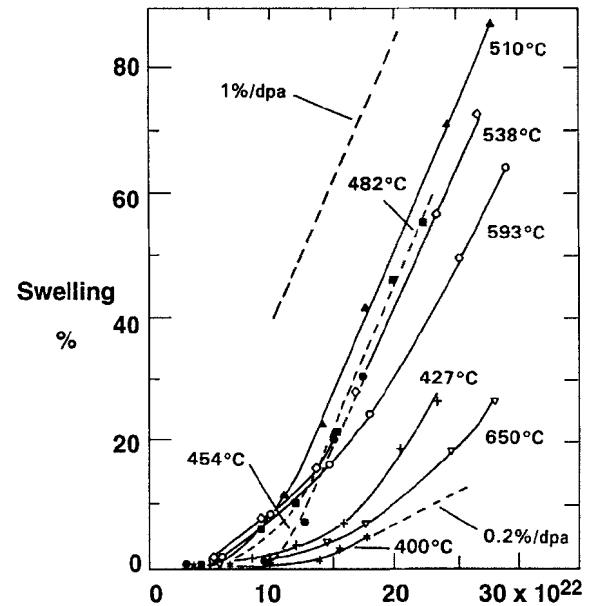
Property	Value
Density	8000 kg/m <sup>3</sup>
Melting T	1390-1440 C
Elastic modulus	193 GPa
Shear modulus	82 GPa



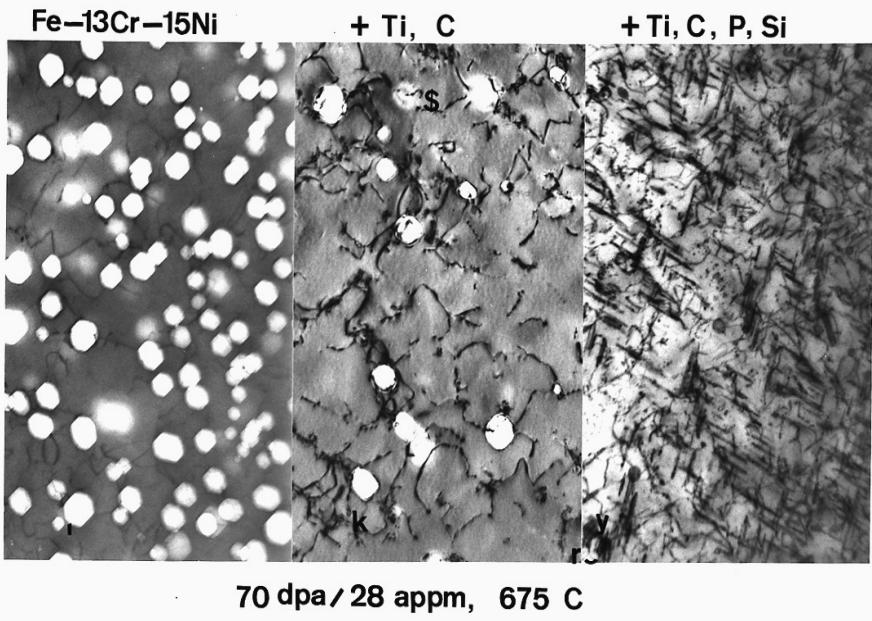
CW316 at 533°C to  
a fluence of 1.5e23  
n/m<sup>2</sup> in the EBR-II.

# Background - Swelling

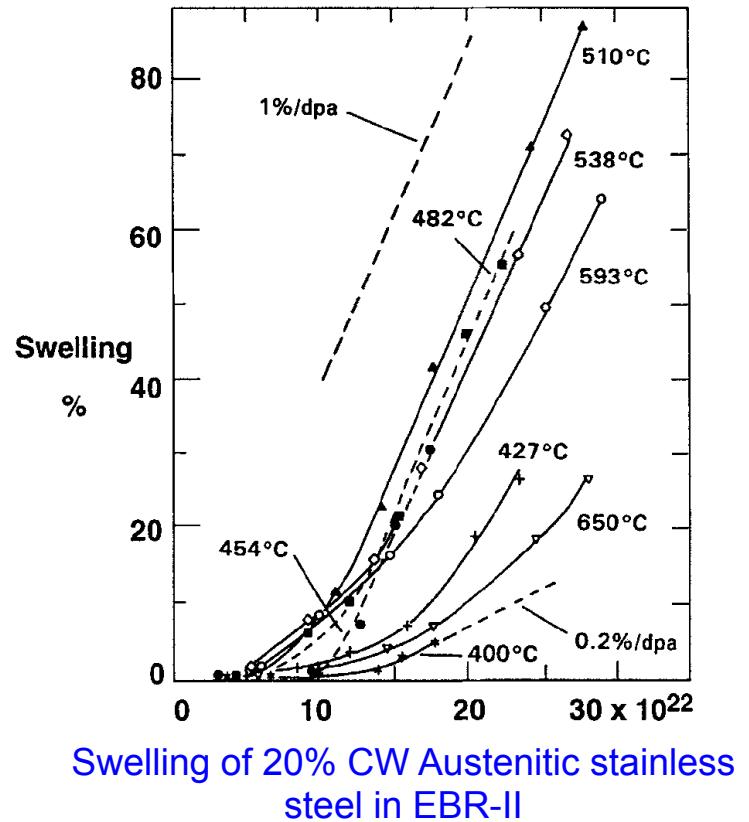
- Dimensional increase of component volume
- Sensitivity to gradients in dose, dose rate and temperature can lead to strong distortions
- Fabricated sizes and shapes not preserved
- May affect particle transport and thermal hydraulics
- Cavity distributions - possible easy paths for fracture
- Limit lifetime



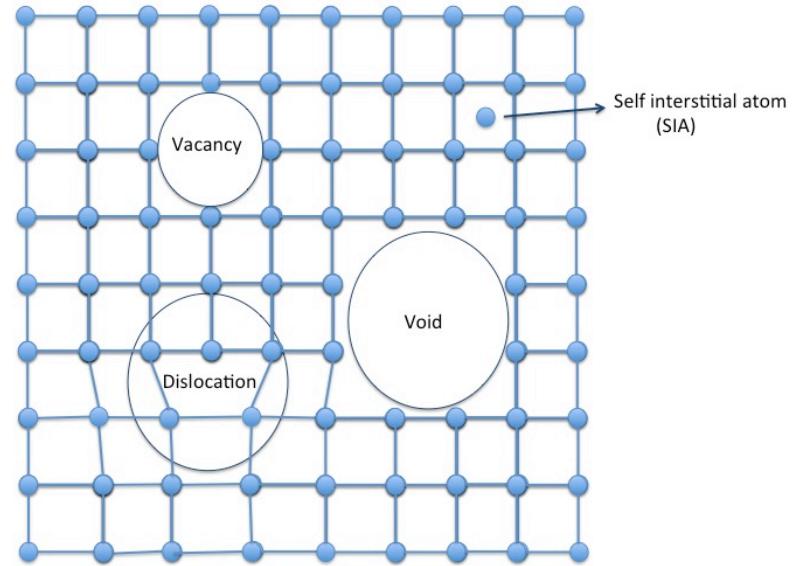
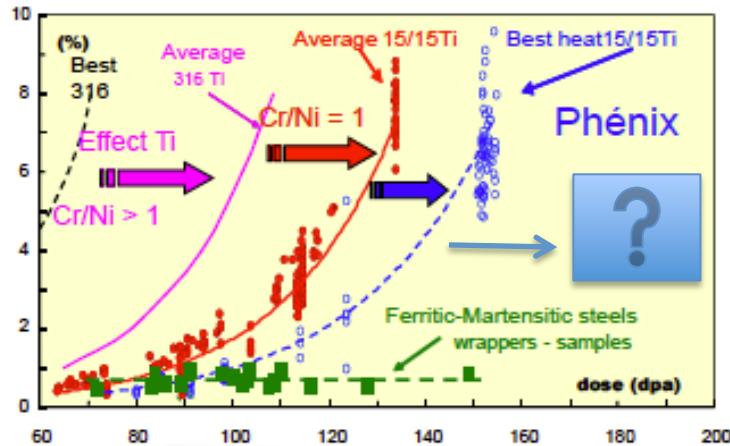
# Why? - Swelling



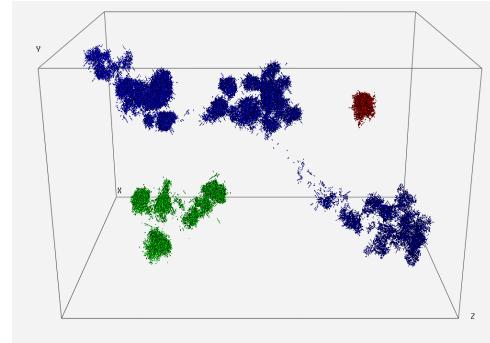
Large reductions in swelling can be attained by alloying additions



# Why? - Swelling



- “Billiard games”
- Primary Knock-on atoms (PKA)
- Collisions in cascades ( $10^{-13}$  s)
- Microstructural evolution ( $10^6$  s)



# How? - Standard Rate Theory

- Traditional rate theory approach:

$$\frac{dC}{dt} = \textit{Generation} - \textit{Annihilation}$$

Disadvantages: Based on mean field approximation

- Diffusion and recombination take place continuously in time and space – defects are uniformly distributed
- Ignores the inhomogeneous nature of defect production in displacement cascades and formation of defect clusters

Advantages:

- Any time scale
- Void swelling from electron radiation (only Frenkel pairs)

# How? - Standard Rate Theory

$$\frac{dC_v}{dt} = G - k_v^2 D_v C_v - \mu_r D_i C_i C_v \quad \frac{dC_i}{dt} = G - k_i^2 D_i C_i - \mu_r D_i C_i C_v$$

Assumptions: Only voids and dislocations are present, recombination is negligible:

$$G - k_C^2 D_v C_v - k_{Dv}^2 D_v C_v = 0 \quad G - k_C^2 D_i C_i - k_{Di}^2 D_i C_i = 0$$

Void is a neutral sink, swelling rate is the net flux of vacancies to voids:

$$\frac{ds}{d\phi} = k_C^2 (D_v C_v - D_i C_i) = B_D \frac{k_C^2 k_{Dv}^2}{(k_C^2 + k_{Dv}^2)(k_C^2 + k_{Di}^2)}$$

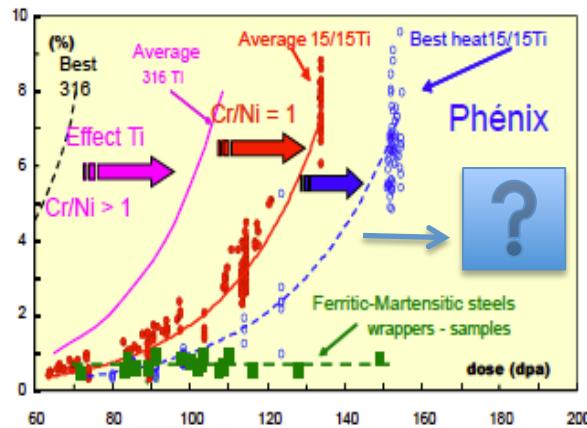
Sink strength  
for voids:

$$k_C^2 = 4\pi \bar{R}N$$

Bias factor:  $B_D = \frac{k_{Di}^2 - k_{Dv}^2}{k_{Dv}^2}$

S total volume of voids;  $\Phi$  irradiation dose;  $k_{v/i}^2$  sink strengths for vacancy / interstitial

# How? – Bias



## Standard Rate Theory (SRT)

Sink bias: different absorption rates of interstitials and vacancies

$$\frac{ds}{d\phi} = B_d \frac{k_c^2 Z_v^d \rho}{(k_c^2 + Z_v^d \rho)(k_c^2 + Z_i^d \rho)}$$

- Analytically
  - Elasticity theory
  - Fick's law with drift term solve diffusion equation
- Experimentally
  - Parameter fitting

Some analytical values:

$$B_D = 25\% \text{ for Cu}$$

$$B_D = 34\% \text{ for Ni}$$

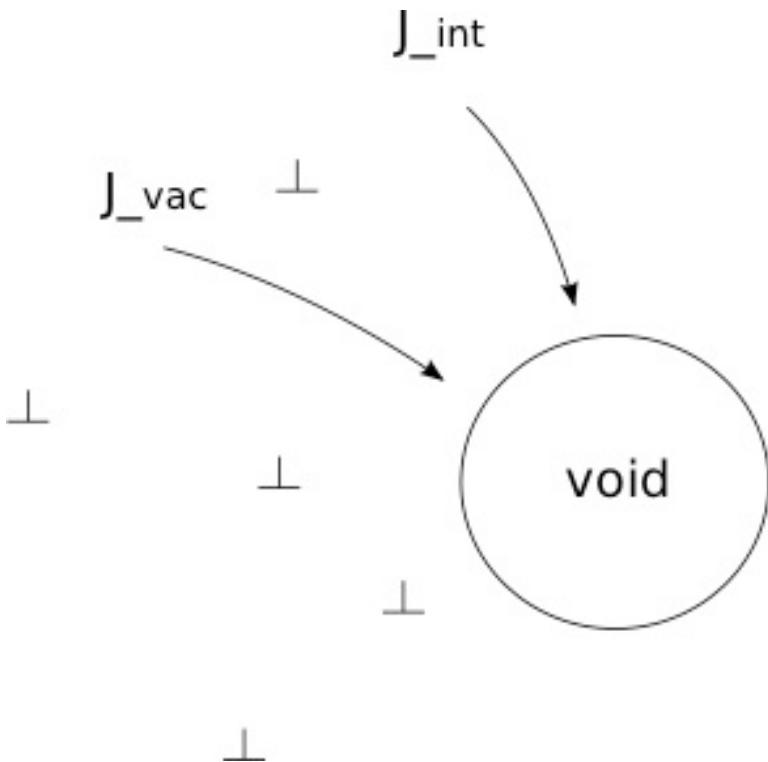
Some experimental values:

$$B_D = 2-4\% \text{ for Cu}$$

$$B_D = 2\% \text{ for pure Fe-Cr-Ni alloy}$$



# How? – Simplest SRT Model



1. Incident particle produces only FPs
2. Both SIAs and vacancies migrate in 3D
3. Dislocations “prefer” SIAs to vacancies.
  - SIAs have stronger interaction energy with dislocation
  - SIAs have larger interaction range

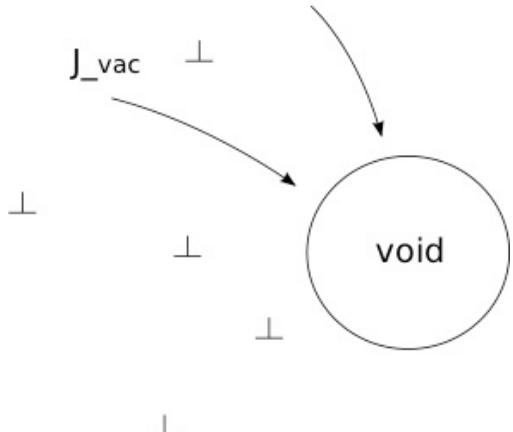
FP =Frenkel pair, SIA=self interstitial atom

# How? - Theoretical approach

$J_{\text{int}}$       Fick's law with drift term:  $J = -\nabla(DC) - \beta DC\nabla E$

$J_{\text{vac}}$       Steady state:  $\nabla J = 0$

$\perp$        $\perp$        $\perp$        $\perp$        $\perp$



$\nabla^2 U = \beta(\nabla U)(\nabla E)$  with  $U = DCE^{B(r)}$

$J = -e^{\beta E(r)} \cdot \nabla U$

$J_{\text{tot}}$  is the total flux around the dislocation core

Sink strength:  $k^2 = \frac{J_{\text{tot}}}{U_\infty - U_0}$

Capture efficiency:  $Z = \frac{k^2}{k_0^2} = \frac{J_{\text{tot}}}{J_0}$

Bias factor:  $B_D = \frac{Z_i - Z_v}{Z_v}$

# How? - Analytical Interactions

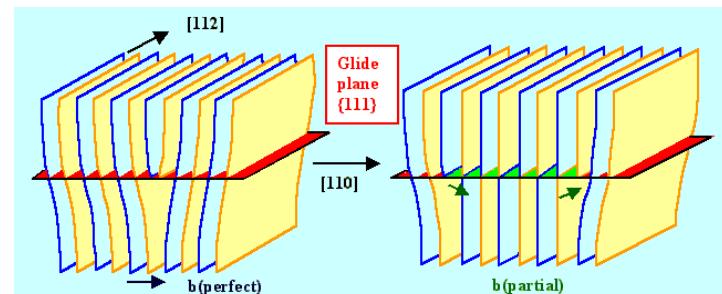
## ➤ 1<sup>st</sup> order size interaction (long range interaction)

- Crystal: elastic medium
- PD: elastic inclusion
- Assumptions:
  - Isotropic system
  - Exact spherical form of PD
  - Non-split dislocation core

$$E(r, \theta) = -\frac{A \sin \theta}{r}$$

$$A = \frac{\mu b}{3\pi} \frac{1+\nu}{1-\nu} \Delta\Omega$$

$\mu$  shear modulus;  $b$  Burgers vector  
 $\nu$  Poisson ratio;  $\Delta\Omega$  dilatation volume



PD=point defects

# How? - Analytical Interactions

## ➤ Anisotropic

- Crystal: **anisotropic** elastic medium
- PD: elastic inclusion

- Assumptions:
  - ~~Isotropic system~~
  - Exact spherical form of PD
  - Non-split dislocation core

$$E(x,y) = \frac{b(1+\nu)I\Delta\Omega}{6\pi} \frac{(2x^2y + Hx^2y + 2y^3)}{(x^2 + y^2)^2 + Hx^2y^2}$$

$$I = (c_{11} + c_{12}) \left[ \frac{c_{66}(c_{11} - c_{12})}{c_{11}(2c_{66} + c_{11} + c_{12})} \right]^{1/2}$$

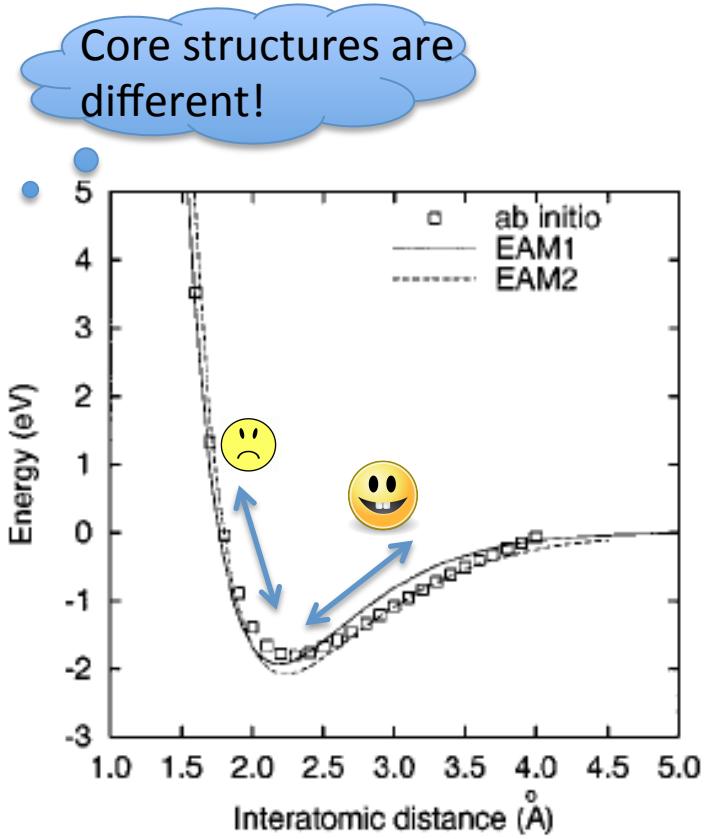
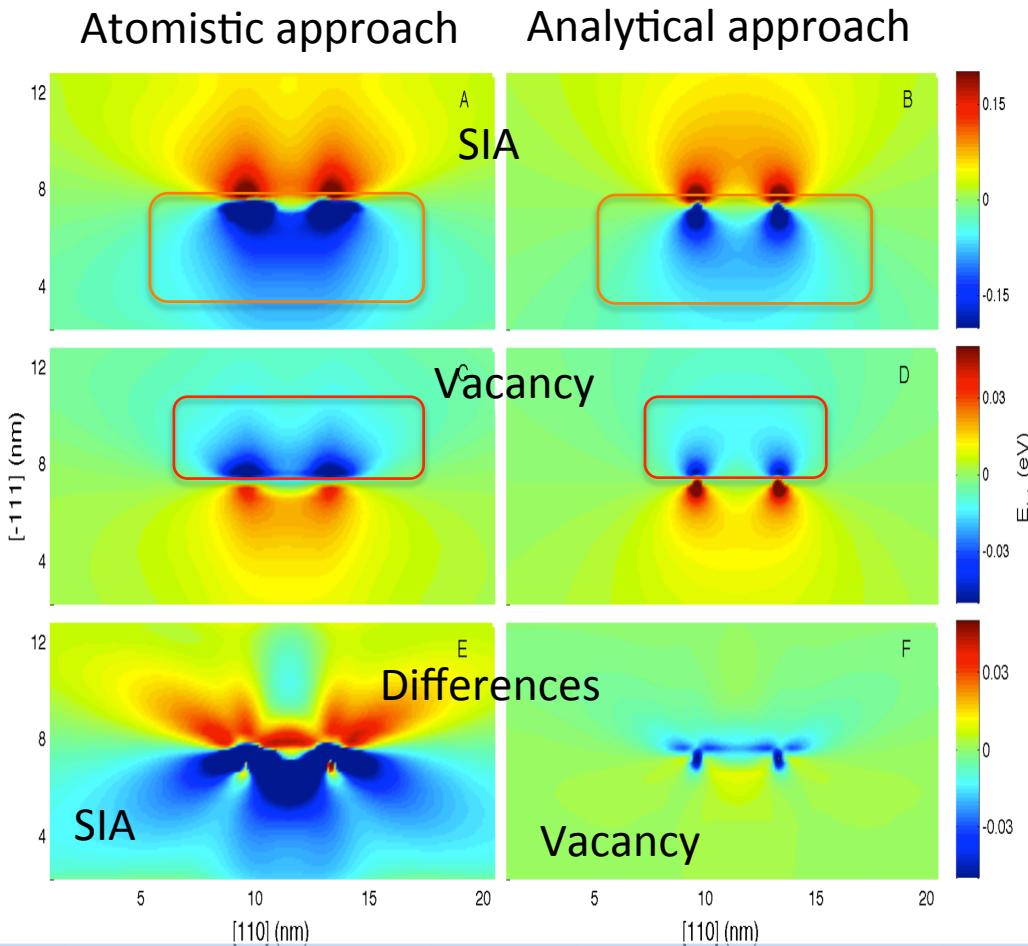
$$H = \frac{(c_{11} + c_{12})(c_{11} - c_{12} - 2c_{66})}{c_{11}c_{66}}$$

b Burges vector;     $c_{ij}$  elastic constants;  
v Poisson ratio;     $\Delta\Omega$  dilatation volume;

# How? - Calculation Methods

- Analytically
    - Elasticity theory
    - Fick's law with drift termsolve diffusion equation analytically
  - Realistically
    - Atomistic model
    - Fick's law with drift termsolve diffusion equation numerically
- 
- | Parameter             | Cu                   | Ni                   |
|-----------------------|----------------------|----------------------|
| $X(a_0)$ [110]        | 70                   | 70                   |
| $Y(a_0)$ [-11-2]      | 7                    | 7                    |
| $Z(a_0)$ [-111]       | 41                   | 76                   |
| Number of atoms       | 85980                | 157572               |
| $\rho_d$ ( $m^{-2}$ ) | $2.8 \times 10^{15}$ | $1.5 \times 10^{15}$ |
- Set up the correct dislocation system
    - Periodic array of dislocation
  - Atomistic calculations
    - DYMOKA package
    - EAM interatomic potential
      - Cu potential from Y. Mishin 2001
        - Stacking fault energy  $44 \text{ mJ/m}^2$
        - Dilatation volume of vacancy:  $-0.3\Omega$ ; of SIA:  $1.8\Omega$
      - Ni potential from G.Bonny 2011
        - Stacking fault energy  $113 \text{ mJ/m}^2$
        - Dilatation volume of vacancy:  $-0.07\Omega$ ; of SIA:  $1.16\Omega$
    - MATLAB PDE toolbox
      - Finite element method, numerical solutions

# What? – Interaction energies Cu

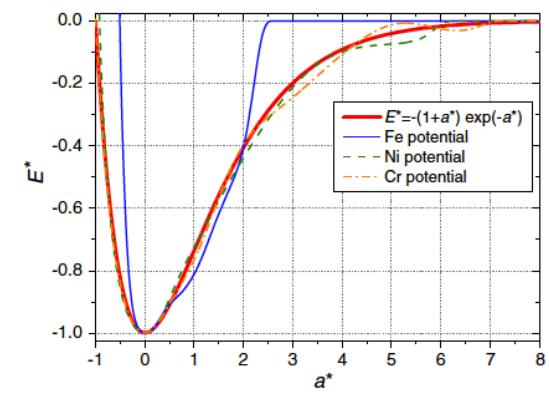
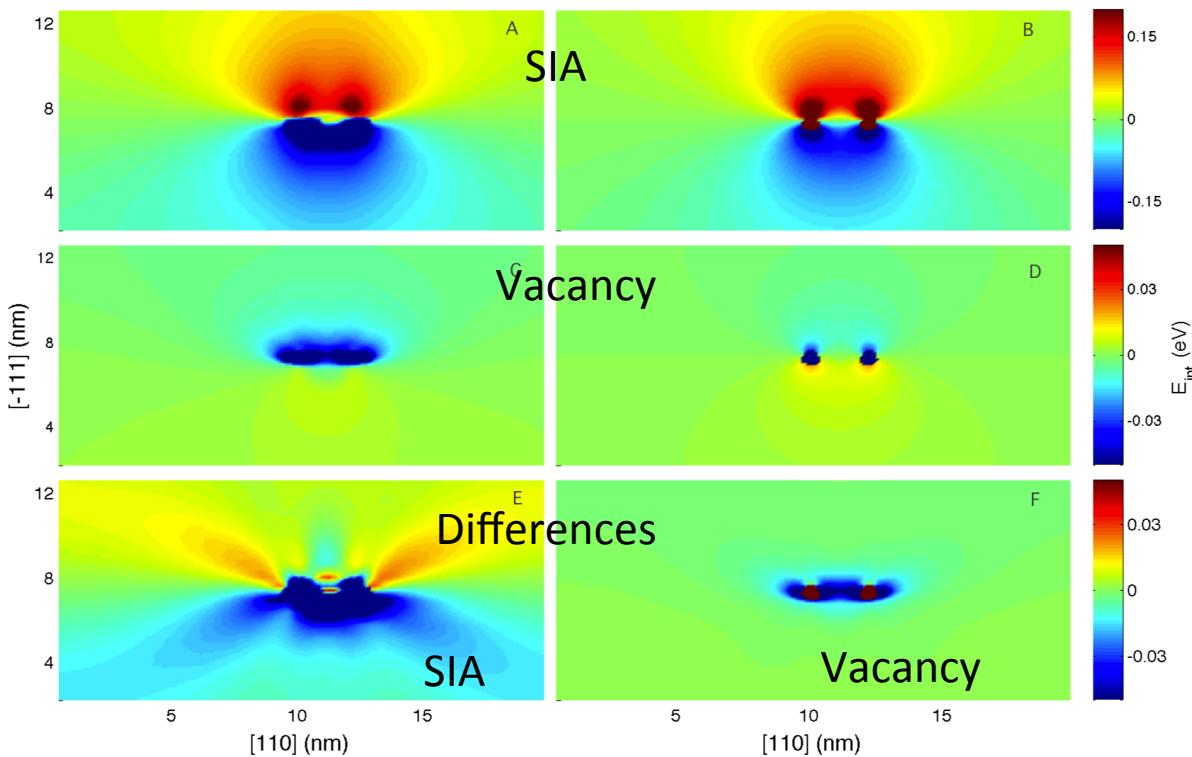


$$E_{SF} = 44.4 \text{ mJ/m}^2 ; d = 37.6 \text{ \AA}$$

Anisotropy: 3.22

# What? – Interaction energies Ni

Atomistic approach      Analytical approach



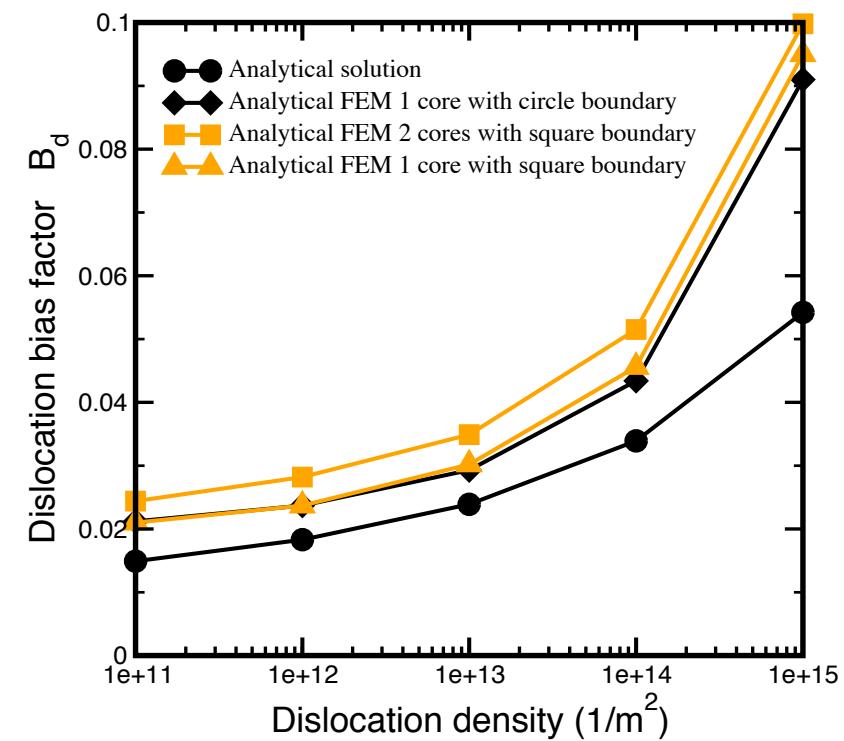
$$E_{SF} = 113 \text{ mJ/m}^2$$

$$d = 22 \text{ \AA}$$

Anisotropy: 2.5

Anisotropic effects;  
Non-linear elasticity;  
First order size interaction;

# What? – Method analysis



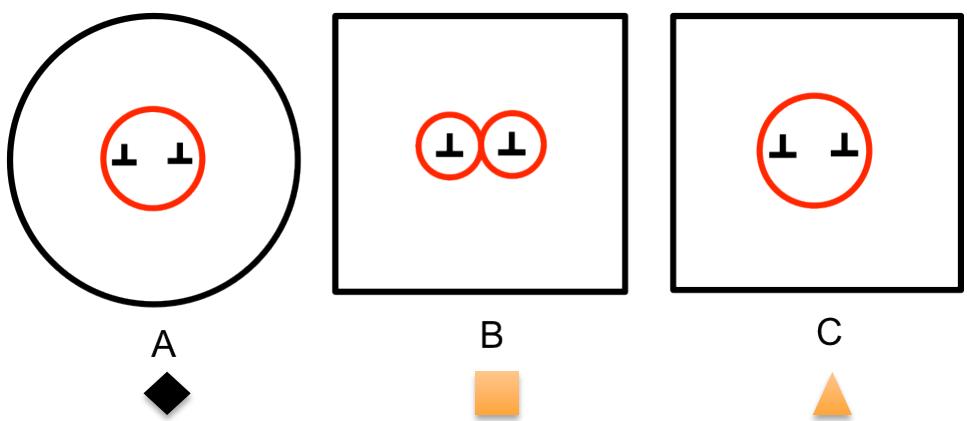
➤ Analytical solution:

$$Z_{\text{str}} = \frac{2\pi I_0(L/2r_0)}{K_0(L/2R_{\text{ext}})I_0(L/2r_0) - K_0(L/2r_0)I_0(L/2R_{\text{ext}})}$$

➤ FEM solutions:

$$z = \oint_{\text{core}} \frac{j(\vec{r})}{j_0} d\vec{r}$$

➤ Different configurations:



# What? – Bias factors

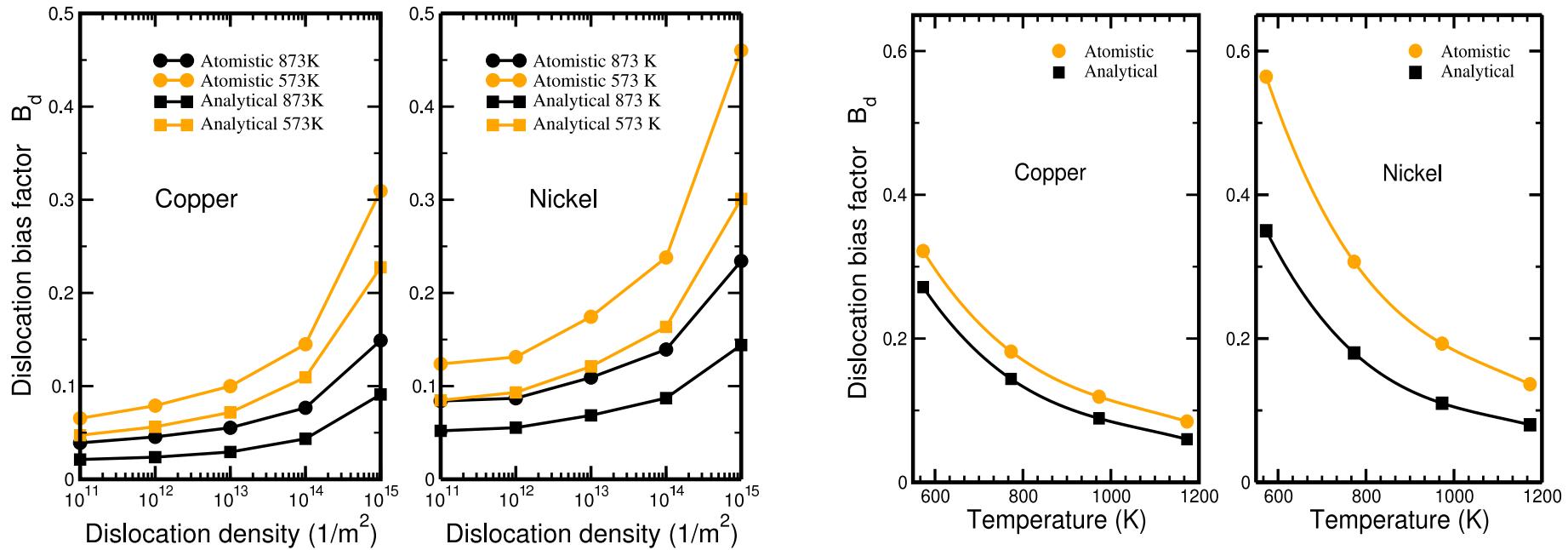
- Cu, Ni @ T=873 K,  $\rho_d = 1.5 \times 10^{15} \text{ m}^{-2}$
- $Z_v^d \sim 1.00$ ,  $Z_i^d$  determine
- $Bd_{Ni} > Bd_{Cu}$
- $Bd_{atom} > Bd_{analytic}$

$$B_D = \frac{Z_i - Z_v}{Z_v}$$

@ 873 K, dislocation density =  $1.5 \times 10^{15} \text{ m}^{-2}$

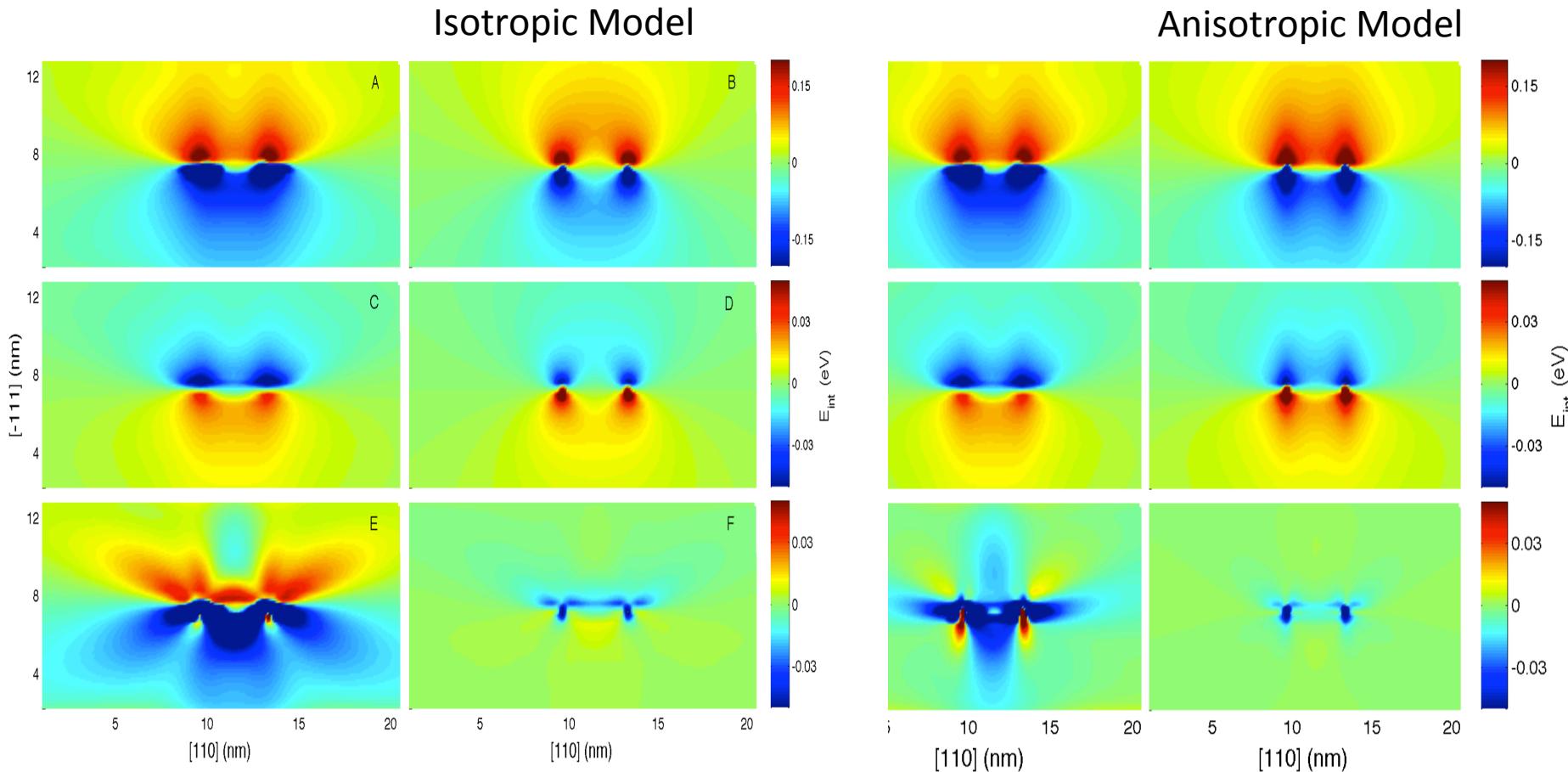
Cu				Ni		
	$Z_i^d$	$Z_v^d$	$B_d$	$Z_i^d$	$Z_v^d$	$B_d$
Atomistic	1.16	1.01	0.15	1.28	1.02	0.25
Analytical	1.12	1.00	0.12	1.16	1.00	0.16

# What? – Bias factors

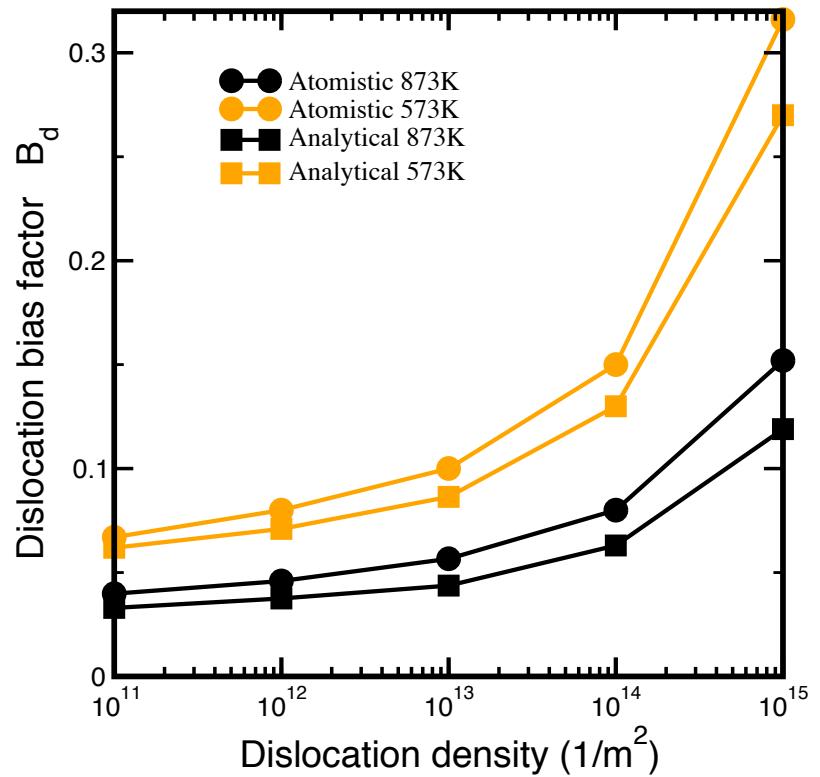
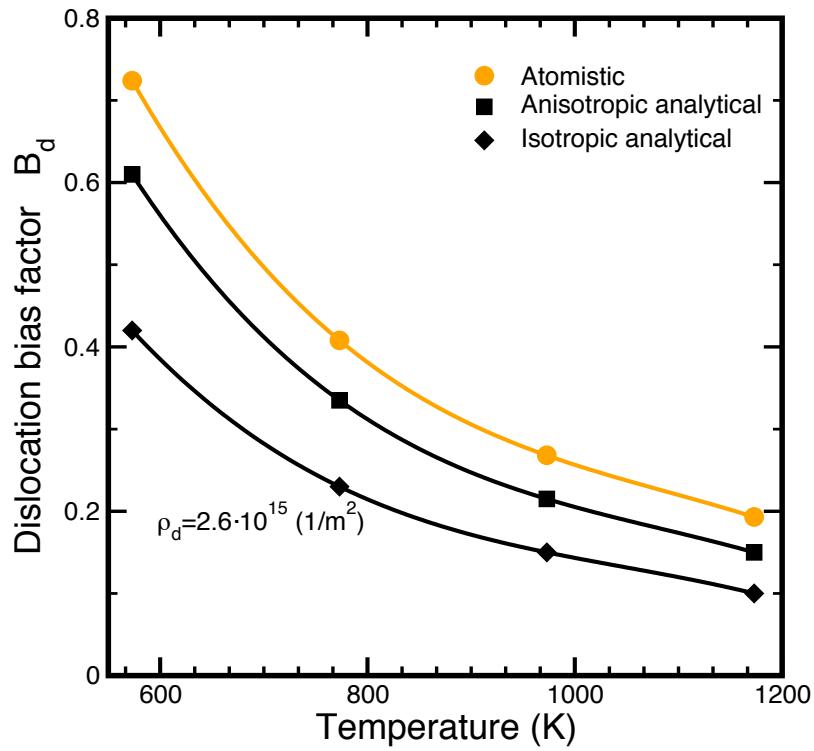


- Density increase,  $B_d$  increase;
- Higher T, lower  $B_d$
- $Bd_{Ni} > Bd_{Cu}$
- $Bd_{\text{atomistic}} > Bd_{\text{analytic}}$
- Low density, high T, atomistic and analytical results tend to converge – Diffusion is dominant.
- High density, low T – core is important.

# What? – Interaction energies Cu



# What? – Anisotropic model in Cu



➤ Anisotropic contribution in Cu

# What? - Comparison

- Cu @ T=520 K,  $\rho_d = 1 * 10^{11} \text{ m}^{-2}$
- Reference calculation: experimental fitting, void size distribution, transient period.
- Atomistic calculation: FEM numerical calculation, mean void size, steady state.

Projectile particle	Dose (dpa)	Void density ( $\text{m}^{-3}$ )	Void diameter (nm)	Reference swelling (%)	Calculated swelling (%)
2.5 MeV Electron	0.013	$0.2-1.2 * 10^{19}$	13.8	$0.2 - 1 * 10^{-3}$	$5.8 * 10^{-3}$
3 MeV Proton	0.002	$9.2 * 10^{19}$	3.9	$2.8 * 10^{-4}$	$5.1 * 10^{-4}$
3 MeV Proton	0.008	$1.3 * 10^{20}$	6.5	$1.9 * 10^{-3}$	$0.91 * 10^{-3}$

# Conclusions

- Atomistic calculation of interaction energy combined with FEM numerical solvation to obtain  $B_d$ .
- SIA has higher interaction energy with dislocation than vacancy, the difference is more significant in atomistic approach than in analytical approach.
- In low T and high dislocation density region, atomic description of dislocation core is in need.
- Atomistic approach predict higher dislocation bias than elasticity theory.
- Anisotropic effect is important.
- Ni is predicted to have larger swelling rate than Cu.
- $B_d >> 2\%$ , not reconcile with the common presumption that dislocation bias is the main driving force for swelling in electron irradiation conditions.

Thank you!